WIPO PCT

P1 1135731

DE OCH WE DESTREAD STREET OF THE COR

<u>TO AVL TO WHOM THESE: PRESENTS SHAM, COMES</u>

UNITED STATES DEPARTMENT OF COMMERCE **United States Patent and Trademark Office**

March 01, 2004

THIS IS TO CERTIFY THAT ANNEXED HERETO IS A TRUE COPY FROM THE RECORDS OF THE UNITED STATES PATENT AND TRADEMARK OFFICE OF THOSE PAPERS OF THE BELOW IDENTIFIED PATENT APPLICATION THAT MET THE REQUIREMENTS TO BE GRANTED A FILING DATE.

APPLICATION NUMBER: 60/436,307 FILING DATE: December 23, 2002

RELATED PCT APPLICATION NUMBER: PCT/US03/40872

By Authority of the COMMISSIONER OF PATENTS AND TRADEMARKS

M. lawer M. TARVER

Certifying Officer

PRIORITY

MPLIANCE WITH RULE 17.1(a) OR (b)



c

•

TELEPHONE 215-563-4100

12-26-02 =5

PTO/SB/16 (10-01)

Approved for use through10/31/2002. OMB 0651-0032

U.S. Patent and Trademark Office; U.S. DEPARTMENT OF COMMERCE

U.S. Patent and Trademark Office; U.S. DEPARTMENT OF COMMERCE

Office of the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number.

PROVISIONAL APPLICATION FOR PATENT COVER SHEET

This is a request for filing a PROVISIONAL APPLICATION FOR PATENT under 37 CFR 1.53(c) Express Mail Label No.

EL 262425164US INVENTOR(S) Given Name (first and middle [if any]) Residence Family Name or Sumame (City and either State or Foreign Country) Thomas **Falke** Hannover, Germany Additional inventors are being named on the separately numbered sheets attached hereto TITLE OF THE INVENTION (500 characters max) "IMPROVING ADHESION BETWEEN TEXTILE REINFORCING MATERIALS AND RUBBER" Direct all correspondence to: CORRESPONDENCE ADDRESS **Customer Number** Place Customer Number Type Customer Number here Bar Code Label here Firm or John S. Child, Jr., Esquire Individual Name DANN DORFMAN HERRELL AND SKILLMAN Address 1601 Market Street, Suite 720 Address City Philadelphia PA 19103 - 2307 State Country United States 215-563-4100 Telephone 215-563-4044 Fax ENCLOSED APPLICATION PARTS (check all that apply) Specification Number of Pages including claims, Abstr CD(s), Number Drawing(s) Number of Sheets Other (specify) Application Data Sheet. See 37 CFR 1.76 METHOD OF PAYMENT OF FILING FEES FOR THIS PROVISIONAL APPLICATION FOR PATENT Applicant claims small entity status. See 37 CFR 1.27. **FILING FEE** X A check or money order is enclosed to cover the filing fees AMOUNT (\$) The Commissioner is hereby authorized to charge filing X fees or credit any overpayment to Deposit Account Number: \$160.00. 04 - 1406Payment by credit card. Form PTO-2038 is attached. æ,.-The Invention was made by an agency of the United States Government or under a contract with an agency of the United States Government. Yes, the name of the U.S. Government agency and the Government contract number are: Respectfully submitted, 12/33/02 Date SIGNATURE REGISTRATION NO. John S. Child, Jr. 28,833 TYPED or PRINTED NAME (if appropriate)

USE ONLY FOR FILING A PROVISIONAL APPLICATION FOR PATENT

Docket Number:

von Kreis.027

This collection of information is required by 37 CFR 1.51. The information is used by the public to file (and by the PTO to process) a complete, including gathering, preparing, and submitting the complete provisional application to the PTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, Washington, D.C. 20231. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Box Provisional Application, Assistant

PROVISIONAL APPLICATION COVER SHEET Additional Page

PTO/SB/16 (10-01)
Approved for use through 10/31/2002. OMB 0651-0032
U.S. Patent and Trademark Office; U.S. DEPARTMENT OF COMMERCE
Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number.

		Docket Nu	ımber	von Kreis.027		
INVENTOR(S)/APPLICANT(S)						
Given Name (first and middle [if any])	Family or Surname		Residence (City and either State or Foreign Country)			
Guenter	Wahl, Dr.		Hohenhameln/Clauen, Germany			
Gerald	Huber,	Dr.	Hannover, Germany			
Andreas	Topp, 1	Dr.	Bielefeld, Germany			
Sadettin	Fidan		Garbsen, Germany			
Jîm	Myers		Waxhaw, North Carolina			
Virgil	Adkins		Charlotte, North Carolina			

Number 2 of 2

WARNING: Information on this form may become public. Credit card information should not be included on this form. Provide credit card information and authorization on PTO-2038.

O

Approved for use through 10/31/2002. OMB 0651-0032
U.S. Patent and Trademark Office; U.S. DEPARTMENT OF COMMERCE
Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number. FEE TRANSMITTAL Complete if Known Application Number for FY 2002 Filing Date Thomas Falke First Named Inventor Patent fees are subject to annual revision. **Examiner Name** Applicant claims small entity status. See 37 CFR 1.27 **Group Art Unit** TOTAL AMOUNT OF PAYMENT (\$) 160.00 Attorney Docket No. von Kreis. 027 METHOD OF PAYMENT (check all that apply) FEE CALCULATION (continued) X Check Credit card Money Order None 3. ADDITIONAL FEES X Deposit Account: Large Entity Small Entity Deposit Account Fee (\$) Fee Fee Code (\$) Fee Code 04-1406 Fee Description Fee Paid Number 105 130 205 Dann Dortman Herrell and Skillman 65 Surcharge - late filing fee or oath Deposit 127 227 25 Surcharge - late provisional filing fee or cover sheet a Commissioner is authorized to: (check all that apply)

Charge fee(s) indicated below

Check all that apply) 139 130 __Charge fee(s) indicated below 139 130 Non-English specification f XCharge any additional fee(s) during the pendency of this application 147 2,520 147 2,520 For filing a request for ex parte reexamination Charge fee(s) indicated below, except for the filing fee 112 112 920° Requesting publication of SIR prior to Examiner action to the above identified deposit account. 113 1,840* 113 1,840* Requesting publication of SIR after Examiner action **FEE CALCULATION** 1. BASIC FILING FEE 115 110 215 55 Extension for reply within first month Large Entity | Small Entity 116 400 216 200 Extension for reply within second month **Fee Description** 117 920 217 460 Extension for reply within third month Code (\$) Code (\$) Fee Paid 118 1,440 101 740 201 370 218 720 Extension for reply within fourth month Utility filing fee 106 330 128 1,960 228 980 206 165 Design filing fee Extension for reply within fifth month 107 510 207 255 Plant filling fee 320 219 160 Notice of Appeal 108 740 208 370 Reissue filing fee 120 320 220 160 Filing a brief in support of an appeal \$160 160 114 214 80 Provisional filing fee 121 280 221 140 Request for oral hearing 138 1,510 138 1.510 Petition to institute a public use proceeding SUBTOTAL (1) (\$) 160.00 140 110 240 55 Petition to revive - unavoidable 2. EXTRA CLAIM FEES FOR UTILITY AND REISSUE 141 1,280 241 640 Petition to revive - unintentional

Fee 110M		_				
Extra Claims below Fee Pa	The time late of outly issue fee (in feissue)	Ī				
Total Claims 200 = X X	143 460 243 230 Design Issue fee	_				
Claims X = X	144 620 244 310 Plant issue fee	_				
Multiple Dependent	122 130 122 130 Petitions to the Commissioner	_				
Large Entity Small Entity	123 50 123 50 Processing fee under 37 CFR 1.17(q)					
Fee Fee Fee Fee Description	126 180 126 180 Submission of Information Disclosure Strnt	_				
Code (\$) Code (\$) 103 18 203 9 Claims in excess of 20	581 40 581 40 Recording each patent assignment per	_				
Olding it excess of 20	property (times number of properties)	_				
102 84 202 42 Independent claims in excess of 3	146 740 246 370 Filing a submission after final rejection					
104 280 204 140 Multiple dependent claim, if not paid	(37 CFR § 1.129(a))					
109 84 209 42 ** Reissue independent claims over original patent	149 740 249 370 For each additional invention to be examined (37 CFR § 1.129(b))					
110 18 210 9 ** Reissue claims in excess of 20 and over original patent	179 740 279 370 Request for Continued Examination (RCE)					
	169 900 169 900 Request for expedited examination of a design application	_				
SUBTOTAL (2) (\$) Other fee (specify)						
**or number previously paid, if greater; For Relssues, see above *Reduced by Basic Filing Fee Paid SUBTOTAL (3)						

SUBMITTED BY

Name (Print|Type)

John S. Child, Jr.

Registration No. (Attornsy/Agent)

Signature

Complete (if epplicable)

125-563-4100

Date

December 23, 2002

WARNING: Information on this form may become public. Credit card information should not be included on this form. Provide credit card information and authorization on PTO-2038.

Burden Hour Statement: This form is estimated to take 0.2 hours to complete. Time will vary depending upon the needs of the individual case. Any comments on the amount of time you are required to complete this form should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, Washington, DC 20231. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Assistant Commissioner for Patents, Washington, DC 20231.

Improving Adhesion between Textile Reinforcing Materials and Rubber

Field of the Invention

5

15

20

25 ·

30

The present invention relates to a method for improving direct adhesion between a textile reinforcing material, e. g., a polyester yarn or cord and an activated rubber. Moreover, the invention relates to a coating composition, a yarn, cord or fabric manufacturing process which is used for the method according to the invention, a textile reinforcing material obtainable by said process having increased adhesion to rubber and a reinforced rubber article having improved dynamic fatigue properties.

10 Background of the Invention

A tire is a highly engineered composite designed to provide safety and durability. Tires, in particular automotive tires for passenger cars or aircrafts, undergo significant dynamic and static stresses and strains in the course of ordinary service life. Performance is a major requirement in this product application due to ramifications of failure while in use. In order to obtain the necessary performance characteristics with regard to the proper functioning of a tire, structural reinforcement like Polyester dtex 1100 – 4400 is a required component of the tire composite. This reinforcement provides many functions in a tire application, in particular overall strength, dimensional stability for the tire and a mechanism to handle stress dissipation during operation (fatigue).

Currently, there is a well established set of products/processes to provide the reinforcing material used in passenger car and truck tire applications.

In order to use textile cords as reinforcing materials, the textile cords are treated with suitable adhesion promoters.

It is a particularly noteworthy fact that, for over more than 70 years, bonding fabric to rubber is still effected with an aqueous dispersion of a resorcinol formaldehyde latex (RFL), with a wide spectrum of choices of resin catalyst (usually caustic and ammonia), in situ and pre-formed resins, molar ratios of resorcinol/formaldehyde (RF), resin/latex (RL) solids ratio, and adhesion-promoting additives. The difficulty in bonding polyester fibers/

to rubber is generally attributed to the presence of only hydroxyl (OH) and carboxyl (COOH) groups at the ends of the polyester molecules, while in nylon (for example) there is a relatively high frequency of amide (CONH) groups along the macromolecular chain. Therefore, this invention is primarily directed to polyester materials, and most particularly to adhesive-activated (AA) polyester fibers in cords, woven, knitted and non-woven fabrics used to reinforce conveyor belts, tires and hose.

5

10

15

20

25

30

Many adhesives and bonding systems ("dips") have been used for fabrics made from synthetic linear polyester yarns. Common systems like glycidyl ethers, phenolic condensates and blocked (or free) polyisocyanates are cost-ineffective and additionally suffer from various other disadvantages like precipitation and instability in baths in which fabrics are dipped. Usually, the fiber producers pre-treat the yarn with finish chemicals (e.g. silanes). Therefore, the resulting adhesive activated (AA) yarns provide an enhanced adhesion with a final adhesion system. This final adhesion system is most often based on RFL (Resorcinol-Formaldehyde-Latex). The adhesion surface on the cord is applied by its dipping in dispersions of RFL. Adhesion between cord and rubber is then achieved during curing with rubber.

Two examples of attempts to improve the adhesion of polyethylene terephthalate filaments to rubber are set forth in United States Patent 3,297,467 and 3,383,242. In these patents, polyethylene terephthalate filaments are treated with a spin finish which is an aqueous dispersion containing a polyglycidic ether of an acyclic hydrocarbon substituted by at least three hydroxyl groups or a diglycidic ether of an aliphatic diol, respectively, in combination with an amine curing agent and a lubricating agent. After heat treatment in order to bind the ether and amine components, the filaments or cord made therefrom can then be treated with an adhesive such as a RFL latex.

United States Patent 3,297,468 describes a similar finish except that the polyglycidic ether is of a cyclic hydrocarbon substituted with at least two hydroxyl groups.

Another example of an epoxide finish additive which may be employed to promote adhesion between a tire cord and an RFL adhesive is disclosed in United States Patent 3,803,035. The finish comprises a lubricating oil, an

antistatic agent, an emulsifier and a polyepoxide. Suitable antistatic agents include quaternary ammonium and pyridinium cationic agents.

United States Patent 3,911,422 and 3,968,304 are directed to a method of bonding polyester tire cords to rubber by use of a two-step process. In the first step, a dip is employed which comprises a low molecular weight polyallyl-glycidyl ether in an aqueous media. In the second step, a dip is employed comprised of an alkaline aqueous dispersion of a rubbery vinyl pyridine copolymer and a resinous composition reactive if exposed to heat.

5

10

15

Also see United States Patent 4,348,517 wherein the same epoxy ether silane is combined with the triglycidyl ether of a glycerol and a defined diglycidyl ether and is used as a fiber finish for polyester yarn.

United States Patent 3,793,425 also describes a process for improving the adhesion of polyester material to rubber. In the process, undrawn polyester yarn is coated with a composition containing an epoxy resin which is preferably buffered with an alkaline agent, such as sodium carbonate, lithium carbonate, potassium carbonate or ammonium hydroxide. The use of epoxy resins with alkaline catalysts to improve the adhesion of polyester to rubber is further disclosed in United States Patent 3,423,230 and United States Patent 3,464,878.

A process for treating chemically stabilized polyester material to improve the 20 adhesion of the polyester to rubber is also described in United States Patent 4,751,143. As noted therein, the aging period for chemically stabilized, adhesive activated polyester material can be reduced by contacting the material before it is substantially drawn or stretched with a composition containing a defined epoxide compound catalyzed with ions of at least one 25 of potassium, cesium, or rubidium at a pH of between about 7.5 to about 13.0. The application of finishes to the polymer surface generally produces a temporary surface condition such as lubrication or electrostatic charge dissipation which may be removed when the surface is subsequently exposed to multiple processing steps. Additionally, polyester surface 30 modifications of the prior art employing epoxies to improve the adhesion of polyester to rubber for example, have resulted in the use of a high level of chemical pick-up. Other approaches employed in art to adjust the characteristics or properties of organic polymer surfaces include electrolytic and plasma treatments. However, these processes are costly and have 35

limited processing rates. The application of a strong acid or base has not been particularly effective in modifying surfaces and can penetrate beyond the surface, particularly in fiber structures, to cause strength loss. Polyisocyanates have been employed to enhance adhesion in the manufacture of polyester yarns (see United States Patent 3,549,740). These materials have been applied at relatively high concentration levels (greater than 0.5 wt.-%) and so generate obnoxious vapors, produce deposits on process rolls and bond filaments to filaments in the yarn bundle. Similar processing problems are encountered in the application of known polyester adhesives such as those based upon resorcinol-formaldehyde resins described in United States Patent 3,660,202 and United States Patent 3,318,750.

5

10

15

20

25

30

United States Patent 4,078,115 discloses an adhesive system for bonding polyester filaments to rubber in which a first coating is employed comprised of the reaction product of a polyepoxide and a quaternized copolymer of 4-vinylpyridine and an aminimide. A second coating of an RFL adhesive is also employed.

Canadian Pat. No. 652,487 discloses a two coat adhesive system. One coat is a composition comprising triallyl cyanurate, the other a composition comprising vinyl pyridine copolymer RFL. The triallyl cyanurate is polymerized prior to bonding to the cord.

United States Patent 3,318,750 also discloses a two coat system. One coat is an aqueous solution of the reaction product of an aldehyde and a composition derived from the reaction of an unsaturated aliphatic ester of cyanuric acid and resorcinol, the other being a RFL dispersion. Optionally the second component can be just the rubbery copolymer latex. The total solid coating is 2% to 7%. This coating is cured, and the cord embedded in rubber and vulcanized.

United States Patent 3,419,463 and United States Patent 3,419,464 also use a reaction product of resorcinol, triallylcyanurate and formaldehyde ("N-3") as part of their adhesive system.

The application of RFL requires considerable expenditure and costs. The Cords are for example treated at high temperatures to cure the adhesive coating which leads to the consumption of a lot of energy, furthermore an

additional process step for the production of tires is needed. In addition the high temperature treating is used to control the balance of the physical properties, such as strength, modulus and shrinkage, of the treated cord.

In order to improve the adhesion further adhesion promoters are added to the rubber in addition to the RFL.

It is known from the prior art that by using a suitable adhesion promoter in sufficient amounts in the rubber formulation adhesion of cords to the rubber can be achieved without applying RFL (direct cord/rubber adhesion). A major disadvantage of this method is the large amount of adhesion promoter needed to achieve the desired effect. As a consequence, the rubber properties are determined to a large extend by the properties of the used adhesion promoter. The large amounts of adhesion-promoters to be used constitute a significant expense factor.

Objects and Summary of the Invention

5

10

- It is therefore a primary object of the present invention to provide an easily applicable and less material consuming method to achieve direct coating to a textile reinforcing fiber during the yarn processing steps. This method should render conventional dipping process as a separate manufacturing step unnecessary.
- A second object of the present invention is the provision of a coating composition which, if applied to the reinforcing material, leads coating (topcoat) providing for an increased adhesion of the coated textile reinforcing material to the rubber compared to the non-coated textile reinforcing material, for instance a yarn.
- A third object of the present invention is the provision of a textile reinforcing material having increased adhesion to rubber.

It is a fourth object of the present invention to provide a reinforced rubber article having improved dynamic fatigue properties.

The method according to the invention provides improved adhesion between a textile reinforcing material, e. g., the textile cord or a reinforcing member, and the rubber of a reinforced article, e. g., a tire, hose, V-belt or a conveyor belt.

Moreover, the method according to the invention leads to a reduction of production expenditure, since a pretreatment of reinforcing material such as a polyester yarn by dipping into adhesion promoters as a separate step during manufacturing, in addition to the elimination of the heat treatment step, is rendered redundant.

In a first embodiment the present invention relates to a method to achieve direct adhesion between a textile reinforcing material and an activated rubber comprising the steps of

5

10

- (A) applying an adhesion-imparting composition to the surface of the textile reinforcing material;
 - (B) exposing the coated textile reinforcing material of step (A) to an elevated temperature;
 - (C) embedding the coated textile reinforcing material of step (B) into an activated rubber; and
- (D) curing the reinforcing material containing rubber obtained from step (C) at a temperature and for a time sufficient to cure said rubber.

In a second embodiment the present invention relates to a coating composition comprising

- 20 (i) a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and
- 25 (ii) a latex having a solids content from about 30 to about 50 wt.-%, preferably about 35 to about 45 wt.-%, most preferably about 41 wt.-%; wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).
- In a third embodiment the present invention relates to a textile reinforcing material obtainable by the method according to the present invention having improved adhesion to rubber. With regard of the present invention "improved adhesion" means that the force (determined according to ASTM 2229-99) which has to be used to pull out the embedded fibers of the

rubber is in the range of at least about 5 to about 10 N, preferably about 15 to about 35 N, most preferably about 20 to about 80 N.

In a fourth embodiment the present invention relates to a reinforced rubber article having improved dynamic fatigue properties. Latter means that the strength of the cords embedded measured after 10.6 million cycles (Disc fatigue test ASTM 6588) was not less than about 60 %, preferably not less than 70 %, most preferably not less than 95 %.

In contrast to the prior art, it has been surprisingly found, that improved adhesion between conventional adhesive activated polyester materials and conventional activated rubbers has been achieved without using conventional resorcinol formaldehyde resins and conventional processes such as dipping and heat treating.

Detailed Description of the Invention

5

10

15

20

25

30

According to the present invention the textile reinforcing material is preferably selected from organic polymeric materials such as polyesters, polyamides, polycarbonates, polynitriles. The polyesters may be selected from any highly polymeric linear polyester obtained by heating one or more glycols of the series HO(CH₂)_nOH, wherein n is greater than 1, but does not exceed 10, with one or more dicarboxylic acid such as naphthalene dicarboxylic acid, 4,4'-diphenyl dicarboxylic acid or preferably terephthalic acid, or an ester forming derivative thereof. Examples of ester forming derivatives of dicarboxylic acids are their aliphatic (including cyclo-aliphatic) and aryl esters and half-esters, its acid halides and their ammonium and salts. Examples of glycols are ethylene, trimethylene, tetramethylene, hexamethylene and decamethylene glycols.

Additionally, the polyester may be reacted or blended with compatible compounds or polymers which do not substantially adversely affect the characteristics of the polyester. For example, compounds yielding non-ester linkages can be added into the reaction mixture for the polyester or pigments, fillers, anti-oxidants, etc. can be blended with the polyester. The preferred polymer for purposes of this invention will be composed of at least about 85 wt.-%, preferably about 95 wt-% polyethylene terephthalate (PET)

or polyethylene naphthalate (PEN) and will most preferably be substantially all polyethylene terephthalate or polyethylene naphthalate.

The material into which the polyester is formed can be any size and configuration amenable to processing which will undergo adhesive activation. The material can therefore be filaments, yarns, cords, fabrics, tapes or films. Preferably, the material is filaments or yarn that is melt spun and quenched, particularly those intended for adhesion to rubber as in the production of tires. Illustrative of such polyester material is multifilament polyethylene terephthalate yarn, which is highly crystalline and highly orientated.

5

10

15

20

25

30

The preparation of such high crystalline and highly orientated yarn is, for example, set forth in United States Patent 4,414,169, the disclosure of which is fully incorporated herein by reference. An alternate process for preparing multiflament polyethylene terephthalate yarn is set forth in United States Patent 4,195,052, the disclosure of which is fully incorporated herein by reference.

The polyester material used in the present invention may or may not be chemically stabilized. Under typical preparation conditions, a polyester, such as polyethylene terephthalate, has a level of carboxyl end groups ranging from about 30 to about 40 microequivalents per gram. To obtain chemical stabilization of the polyester, a compound such as ethylene carbonate, phenyl glycidyl ether, or preferably ethylene oxide, is incorporated into the polyester material. For example, ethylene oxide can be added to a polyester melt which is maintained at a pressure of from about 3,548 kPa to about 35,480 kPa in accordance with the disclosures of United States Patents 4,016,142 and 4,442,058, the disclosure of each of which is fully incorporated herein by reference.

Although the invention is described in terms of the adhesive activating of polyester material, it will be appreciated that other polymers which may be activated by the present activator systems may likewise be treated. Such polymers include polyamides, especially aromatic polyamides (e.g., Kevlar), nylon, polycarbonate, rayon and other textile reinforcing fibers.

The term "filament" or "fiber", as used herein, refers to the components which make up a yarn.

The term "yarn", as used herein, is a generic term for a continuous strand of fibers, or filaments.

The term "cord" as used herein refers to a plurality of polyester filaments or yarns twisted together to form a single string or reinforcement element. In one illustrated embodiment, the cord comprises 2 to 3 yarns, has a linear density of dtex about 2200 to about 8800, a twist multiplier of about 2.0 to 7.5 (turns per meter/ $\sqrt{\text{dtex}}$).

The cord of the invention is preferably made of polyester such as polyethylene terephthalate (PET) or polyethylene naphthalate (PEN).

The polyester yarns applied in the present invention are preferably adhesive activated yarns having high-modulus-low-shrink (HMLS) properties. Such yarn having a high modulus, preferably less than about 5% elongation at a load of about 40 cN/tex. They are manufactured by high speed spinning followed by applying a finish comprising epoxy-compounds as described in GB-A-1012935, European published patent application 0420333 and United States Patent 3,775,150 or halohydroxy compounds as described in United States Patent 5,328,765, the disclosure of each of which is fully incorporated herein by reference. Afterwards the yarn is drawn and heat-treated.

20 (A) Application of the Topcoat

5

The textile reinforcing material is coated on its surface by contacting the material after it has been drawn and/or heat set with a coating composition comprising

- (i) a resin obtainable by the reaction of triallyl cyanurate and resorcinol at temperatures from about 180 to about 280°C, preferably about 200 to about 260°C, most preferably about 220 to about 240°C then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia;
 - (ii) a latex;

ţ

wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

The coating composition can be an aqueous, a non-aqueous or an emulsion composition which comprises at least one polymerizable component. The reinforcing material is surface-treated/coated with said coating composition thus forming a top-coat which, after the removal/evaporation of the solvents leaves behind a coating on the surface of the reinforcing material which gives raise to an improved adhesion to rubbers, in particular activated rubbers.

5

10

15

20

Suitable resin components (i) are well known in the art under the designation "N-3", e.g. from United States Patent 3,318,750 and 3,419,464 and Canadian patent application 652,487, the disclosure of each of which is fully incorporated herein by reference.

The latex component (ii) of this invention should not be considered as being limited to any specific type of synthetic rubber latex, but rather to include all of those comparable diene polymer latex compositions commonly employed in the rubber fabricating industry. It is preferred however, that the latex contains at least some vinyl pyridine latex. This well-known type of latex is formed from butadiene, styrene, and vinyl pyridine monomers, in a ratio of about 50 to about 80 wt.-% of butadiene, about and about 10 to about 25 wt.-% of vinyl pyridine monomers, usually in a ratio of about 70/15/15 wt.-%.

The coating composition may further comprise a lubricant, such as butyl stearate, ethoxylated long chain alcohols, ethoxylated polysiloxanes and mixtures thereof, in amounts ranging from about 0 to about 1% by dry weight.

The coating composition may also comprise a solvent, such as water, acetone, butyl carbitol, isopropanol, ethanol and mixtures thereof. The preferred solvent is water in an amount ranging from about 1 to about 99 %, preferably about 50 to about 95 % by weight. Water is advantageously employed as the solvent for a composition used as a coating on drawn yarn.

Other components which may be present in the coating composition include tints, fluorescent brighteners, emulsifiers, antifoaming agents, antimicrobial compounds, co-catalysts, flexibilizers such as methacrylates and mixtures thereof. The total amount of solids (i.e., all constituents except solvent) in

the topcoat composition typically ranges from about 1 to about 90% by weight, preferably from about 1 to about 50% by weight.

The coating composition can be applied to the polymeric material using any suitable means which is selected primarily based on the form of the material. Exemplary means include a metered applicator, a kiss roll, spray or foam and results in a coating level with increasing preference in the order given of at least about 0.01, 0.05, 0.1 % by weight. The coating level can be – with increasing preference in the order given – up to about 3 %, 2 %, 1.5 % and 1% by weight, based on the weight of the dry coated textile reinforcing material.

Polymerizing Step (B)

5

10

15

20

25

30

After applying the coating composition to the drawn yarn or cord it is at least partially polymerized by exposing it to an elevated temperature sufficiently high to polymerize polymerizable constituents contained in the coating composition. It is preferred to expose the coated textile reinforcing material to a temperature of from about 110 to 235° C. The exposure time at lower temperatures is several minutes, at higher temperatures it is about 60 seconds or less. At least partially polymerizing means in accordance with the present Invention that at least about 5 to about 50 mol-%, preferably about 10 to about 30 mol-%, most preferably about 15 to about 25 mol-% of the monomers are linked with each other. Optionally this polymerization step can be conducted in the normal treating process.

Curing Step (C)

After at least partially polymerizing the coating composition the coated textile reinforcing material embedded into the rubber matrix resulting in an adhesion of the rubber to the reinforcing material. Therefore, the coated polymeric reinforcing material, for instance, a polyester cord/yarn is embedded in a curable rubber and the rubber is cured for about 6 to 120 min, preferably for about 6 to about 15 min., most preferred for about 6 to about 10 min. at temperatures of about 160 to about 200°C, preferably of about 160 to about 190°C, most preferred of about 170 to about 180°C.

In a preferred embodiment of the present invention the rubber employed is an activated rubber, i.e., a rubber formulation which comprises agents known from the prior art for improving the adhesion to RFL treated cord. Specific examples for said rubber adhesion promoters are resorcinol, hexamethoxymethyl melamine (HMMA), sulfur, sulfenamides, zinc oxide, stearic acid and carbon black.

The term "rubber" as used herein refers to carbon black and/or silica filled 5 natural and synthetic rubber systems, which can be cured so as to exhibit elastomeric properties. For the purpose of this invention the term "elastomer" is used interchangeably with the term "rubber". Representative synthetic rubbery polymers include the diene polymers. Diene polymers 10 comprise those polymers having rubber-like properties which are prepared by polymerizing a conjugated C₄ to C₆ diolefin such as butadiene, isoprene chloroprene copolymerized with styrene, methyl styrene and acrylonitrile, the conjugated diolefin usually being present in the mixture to the extent of at least about 40 wt.-% - based on the total of polymerizable material - and 15 preferably in major portion. The butadiene-styrene copolymers are manufactured commercially under such names as SBR 1000, SBR 1006, SBR 1500 and 1502.

Other synthetic rubbers include the "neoprene" rubbers. "Neoprene" is a generic name which is applied to polymers of chloroprene, and copolymers of chloroprene with dienes or vinyl compounds, in which the chloroprene comprises the predominant monomer. An isobutylene-isoprene copolymer "Butyl" rubber, as well as the elastomeric ethylene-propylene copolymers and terpolymers may also be used.

20

25

The term "cured" is used interchangeably with the term "vulcanized" in conjunction with the cured rubber component of this invention denotes that the rubber component to be vulcanized has been cured to a state in which the physical properties of the rubber are developed to impart elastomeric properties to the rubber generally associated with the rubber in its conventional vulcanized state.

The rubber employed may contain customary amounts of various conventional additives such as those needed to effect or accelerate vulcanization. Examples of such materials include sulfur, sulfur chloride, sulfur thiocyanate, thiuram polysulfides and other organic or inorganic polysulfides. These components are preferably employed in amounts

varying from about 0.1 to about 10 wt.-% and preferably from about 0.3 to about 3 wt.-% of rubber.

Many other materials may also be included in the rubber composition such as pigments, antioxidants and the like, all in accordance with practices well known in the art.

The following Examples are given as illustrations of the invention. It should be understood, however, that the invention is not limited to the specific details set forth in the Examples.

The following examples are presented to illustrate the invention which is not intended to be considered as being limited thereto. In the examples and throughout percentages are by weight unless otherwise indicated.

While in accordance with the patent statutes, the best mode and preferred embodiment have been set forth, the scope of the invention is not limited thereto, but rather by the scope of the attached claims.

15 Examples

5

Commercial HMLS tire yarns from KoSa were used for the Examples. Type 792 is a non-adhesive activated yarn, Type 793 is an adhesive activated (AA) (halohydroxy based) yarn and Type 748 is another adhesive activated yarn (epoxy based).

20 The topcoat composition (N3-L) used in the examples was

35.7 wt.-% butadiene/styrene/vinylpyridine terpolymer (Gentac 118® from Omnova Solutions Inc., Mogadore Ohio, USA);

35.7 wt.-% N-3® from FCI Technology Inc. Bessemer City, North Carolina, USA.

25 28.6 wt.-% Water

The yarns or cords were coated to a total level of finish on yarn, unless otherwise stated, of 1.0 wt.-% on a dry weight basis.

The coated/treated yarns or cords were heated at 229° for 60 seconds, unless otherwise stated. The rubbers used in the examples were Rubber A a non-activated rubber (without resorcinol and formaldehyde and Rubber B an activated rubber (containing resorcinol and formaldehyde).

Example 1

1440 dtex Type 792 and 793 yarns were twisted into a 2 ply cord with a twist multiplier of 6. These cords were coated and partially polymerized for 55 seconds at 235° C and then embedded in both activated and non-activated rubbers and cured at 150° C for 30 minutes. The force to pull out the cords was measured according to ASTM 2229-99, and the results set forth in Table 1.

Table 1

10

15

5

Yarn (PET)	Rubber	Pull-out Adhesion (N)
792 (non-AA)	Α	15
792 (non-AA)	В	25
793 (AA)	Α	20
793 (AA)	В	65-85

The results in table 1 demonstrate that the combination of AA-Yarn and activated Rubber B lead to a significant increase of adhesion level. The results of 792 yarn in Rubber A represent the prior art of United States Patent 3,318,750.

Only if the rubber contains an adhesion promoter and the cord contains an active finish, significant levels of adhesion could be observed in the pull-out test.

In accordance to the present invention it has been observed, that it was sufficient to use a standard topcoat (on the yarn) and small amounts of a standard adhesion system in the rubber to achieve good adhesion. The topcoat is interacting directly with the rubber and not via the RFL.

Example 2

The adhesion of the inventive system was compared to conventional RFL dipping. Fabrics (121 epdm) were prepared from Type 793 and Type 748

cords. Both the 793 and 748 fabrics were coated with the N3-L topcoat and partially polymerized prior to the fabric being embedded in activated rubber B. One length of 793 fabric was not coated, and another dipped in a standard RFL composition with a 5% dip pick-up and cured. The rubber composite was cured for 10 min. at 177°C. The peel adhesion (ASTM 4393) of these composites is set forth in Table 2.

This example shows that the cord material obtained from coated yarns has equivalent adhesion forces compared to standard RFL dipped cords. In addition, the coated samples show a significant adhesion improvement compared to the non-coated sample.

Table 2

Yarn in Fabric	Peel Adhesion Force (N)		
793 (non-coated)	65-98		
793 (coated)	135-152		
793 (dipped)	132-178		
748 (coated)	145-159		

Example 3

5

10

15 The fabrics for Example 2 were used to build 205/60 R15 tires. The peel adhesion of sections cut from the sidewalls was measured and the results set forth in Table 3.

Table 3

Yarn in Fabric	%Rubber Coverage	Adhesion (N)
793 (non-coated)	· 0	38-46
793 (coated)	10	42-54
793 (dipped)	70	53-60
748 (coated)	80	72-81

Table 3 shows the in-tire adhesion performance of calendered carcass fabrics. With all activated Rubber B skim compound the cured tire shows, under equivalent curing conditions, that coated and dipped carcass sections show equivalent adhesion performance, and low adhesion values in the case of tires built with non-coated 793. Best results for rubber coverage shows in tire cord fabric manufactured with coated 748 (AA) yarn.

10 Testing of these tires, high speed, endurance and durability in the flexing zone showed no difference between the fabrics.

Example 4

The effect of the curing conditions on the final adhesion (pull-out force) between rubber and cord was measured using cords from Example 1, and the results set forth in Table 4. As is evident from the results, longer curing-times and higher temperatures are beneficial to achieve higher adhesion. Preferably, curing temperatures of 160-200°C are applied, the cure time may be varied between 6-120 min.

Table 4
Pull-out Adhesion (N)

Yarn	Curing Conditions (in Rubber B)						
	30 min @150°C	1	ł	15 min @170°C	1	12 min @180°C	15 min @180°C
793	34	33	53	65	44	54	55
748	45	43	73	78	70	92	86

5 Example 5

The topcoat was applied at various stages of the process:

- A) Yarn coated and then twisted into 2-ply cord
- B) Yarn twisted into a single ply, coated and twisted into a 2-ply cord
- C) Cord coated
- The cords were partially polymerized, embedded in rubber B and cured. The peel force of the cured rubber was measured and the results set forth in table 5.

Table 5

Application process	Yarn Type	Pull-out Adhesion (N)
Α	793	30
В	793	40
С	793	62
Α	748	72
В	748	30
С	748	93

The preferred method for applying the topcoat is either at the yarn or cord stage.

Example 6

5 1440 dtex Type 748 yarns were coated with 0.6wt.% of N3-L, and partially polymerized for 11 seconds at 220° C. The yarns were twisted into 2-ply cords at a low twist level of 250. Control cords from the same yarn were prepared at different twist levels and dipped in a standard RFL dip composition with a 5% dip pick-up and cured in a treating oven. These cord were embedded in the activated Rubber B and cured at 150° C for 30 minutes.

Visual inspection of the cords after a peel adhesion test showed excellent adhesion of the cords (visual ratings of 4.5 to 5).

The embedded cords were subjected to a dynamic fatigue test (Disc fatigue test ASTM 6588), and the strength of the cords measured after 3.6 and 10.6 million cycles. The results are set forth in Table 6 below.

Table 6

Adhesion System	Twist level (Turns/meter)	Retained strength, % (Number of cycles)	
	, ,	3.6 million	10.6 million
RFL	370	100	94
RFL	310	92	82
RFL	250	75	47
N3-L	250	95	70

20

This demonstrates the superior dynamic fatigue of the inventive system, and will allow lower twist levels to be used in rubber composites.

What is claimed is:

- 1. A method to achieve direct adhesion between a textile reinforcing material and an activated rubber comprising the steps of
 - (A) applying an adhesion-imparting composition to the surface of the textile reinforcing material;
 - (B) exposing the coated textile reinforcing material of step (A) to an elevated temperature;
 - (C) embedding the coated textile reinforcing material of step (B) into an activated rubber; and
- 10 (D) curing the reinforcing material containing rubber obtained from step (C) at a temperature and for a time sufficient to cure said rubber.
- 2. The method of claim 1 wherein the adhesion-imparting composition is an aqueous composition.
 - 3. The method of claim 1 wherein the adhesion-imparting composition comprises at least one polymerizable component.
- 20 4. The method of claim 1 wherein the textile reinforcing material is an organic polymeric material.
- 5. The method of claim 4 wherein the textile reinforcing material is selected from the group of aliphatic and aromatic polyesters, polyamides, polycarbonates and rayon.
 - 6. The method of claim 1 wherein the coated textile reinforcing material is exposed to a temperature in the range of from about 110°C to about 250°C;

- 7. The method of claim 1 wherein the rubber is selected from the group consisting of diene rubbers, diene/alpha-olefin rubbers, ethylene/propylene rubbers and ethylene/alpha-olefin/diene rubbers.
- The method of claim 1 wherein the rubber is cured at a temperature of from about 140°C to 220°C, preferably from about 160°C to 200 °C, most preferably from about 170 °C to 180°C.
- 9. The method according to claim 1, wherein the adhesion-imparting composition comprises

15

- i. a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and
- ii. a latex having a solids content from about 30 to about 50 wt.-%, preferably about 35 to 45 wt.-%, most preferably about 41 wt.-% wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).
- 10. A treating composition for imparting adhesion to reinforcing materials said composition comprising
- i. a resin having a solids content from about 10 to about 50 wt.-%,
 preferably from about 15 to about 30 wt.-%, most preferably
 from about 20 wt.-% obtainable by the reaction of triallyl
 cyanurates and resorcinol at high temperatures, then reacting the
 resulting product with formaldehyde and solubilizing it in aqueous
 ammonia; and
- ii. a latex having a solids content of from about 30 to about 50 wt.-%, preferably about 35 to 45 wt.-%, most preferably about 41 wt.-%

wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

- 5 11. A textile reinforcing material obtainable by a method comprising the steps of
 - (A) applying an adhesion-imparting composition to the surface of the textile reinforcing material; and
- (B) exposing the coated textile reinforcing material of step (A) to an elevated temperature.
 - 12. The material of claim 11 wherein the adhesion-imparting composition is an aqueous composition.
- 15 13. The material of claim 11 wherein the adhesion-imparting composition comprises at least one polymerizable component.

- 14. The material of claim 11 wherein the textile reinforcing material is an organic polymeric material.
- 15. The material of claim 14 wherein the textile reinforcing material is selected from the group of aliphatic and aromatic polyesters, polyamide, polycarbonate and rayon.
- 25 16. The material of claim 11 wherein the coated textile, reinforcing material is exposed to a temperature in the range of from about 110°C to about 250°C;
- 17. The material of claim 11 wherein the adhesion-imparting composition comprises

- i. a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and
- ii. a latex having a solids content from about 30 to about 50 wt.-%, preferably about 35 to 45 wt.-%, most preferably about 41 wt.-%
- wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).
 - 18. The material of claim 11 wherein the adhesive coating is present in an amount of from about 0.01 to about 3 % by weight, preferably from about 0.05 to about 2 % by weight, and most preferably from about 0.1 to about 1.5 % by weight, based on the weight of the dry coated textile reinforcing material.
- 19. A reinforced rubber article having improved dynamic fatigue
 20 properties obtainable by a method comprising the steps of
 - (A) applying an adhesion-imparting composition to the surface of the textile reinforcing material;
 - (B) exposing the coated textile reinforcing material of step (A) to an elevated temperature;
- (C) embedding the coated textile reinforcing material of step (B) into an activated rubber; and
 - (D) curing the reinforcing material containing rubber obtained from step (C) at a temperature and for a time sufficient to cure said rubber.

30

5

15

20. The article of claim 19 wherein the adhesion-imparting composition is an aqueous composition.

- 21. The article of claim 19 wherein the adhesion-imparting composition comprises at least one polymerizable component.
- 5 22. The article of claim 19 wherein the textile reinforcing material is an organic polymeric material.
- 23. The article of claim 19 wherein the textile reinforcing material is selected from the group of aliphatic and aromatic polyesters, polyamides, polycarbonates and rayon.
 - 24. The article of claim 19 wherein the coated textile reinforcing material is exposed to a temperature in the range of from about 110°C to about 250°C;

15

- 25. The article of claim 19 wherein the rubber is selected from the group consisting of diene rubbers, diene/alpha-olefin rubbers, ethylene/propylene rubbers and ethylene/alpha-olefin/diene rubbers.
- 20 26. The article of claim 19 wherein the rubber is cured at a temperature of from about 140°C to 220°C, preferably from about 160°C to 200 °C, most preferably from about 170 °C to 180°C.
- 27. The article according to claim 19, wherein the adhesion-imparting composition applied comprises
 - i. a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and

ii. a latex having a solids content from about 30 to about 50 wt.-%, preferably about 35 to 45 wt.-%, most preferably about 41 wt.-% wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

5

10

28. The article of claim 19 wherein the adhesive coating is present in an amount of from about 0.01 to about 3 % by weight, preferably from about 0.05 to about 2 % by weight, and most preferably from about 0.1 to about 1.5 % by weight, based on the weight of the dry coated textile reinforcing material.

Abstract

Improving Adhesion between Textile Reinforcing Materials and Rubber

The present invention relates to a method for improving direct adhesion between a textile reinforcing material and an activated rubber. Moreover, the invention relates to a coating composition, a yarn, cord or fabric manufacturing process which is used for the method according to the invention, a textile reinforcing material obtainable by said method having increased adhesion to rubber and a reinforced rubber article having improved dynamic fatigue properties.

Improving Adhesion between Textile Reinforcing Materials and Rubber

Field of the Invention

5

15

20

25

30

The present invention relates to a method for improving direct adhesion between a textile reinforcing material, e. g., a polyester yarn or cord and an activated rubber. Moreover, the invention relates to a coating composition, a yarn, cord or fabric manufacturing process which is used for the method according to the invention, a textile reinforcing material obtainable by said process having increased adhesion to rubber and a reinforced rubber article having improved dynamic fatigue properties.

10 Background of the Invention

A tire is a highly engineered composite designed to provide safety and durability. Tires, in particular automotive tires for passenger cars or aircrafts, undergo significant dynamic and static stresses and strains in the course of ordinary service life. Performance is a major requirement in this product application due to ramifications of failure while in use. In order to obtain the necessary performance characteristics with regard to the proper functioning of a tire, structural reinforcement like Polyester dtex 1100 – 4400 is a required component of the tire composite. This reinforcement provides many functions in a tire application, in particular overall strength, dimensional stability for the tire and a mechanism to handle stress dissipation during operation (fatigue).

Currently, there is a well established set of products/processes to provide the reinforcing material used in passenger car and truck tire applications.

In order to use textile cords as reinforcing materials, the textile cords are treated with suitable adhesion promoters.

It is a particularly noteworthy fact that, for over more than 70 years, bonding fabric to rubber is still effected with an aqueous dispersion of a resorcinol formaldehyde latex (RFL), with a wide spectrum of choices of resin catalyst (usually caustic and ammonia), in situ and pre-formed resins, molar ratios of resorcinol/formaldehyde (RF), resin/latex (RL) solids ratio, and adhesion-promoting additives. The difficulty in bonding polyester fibers

to rubber is generally attributed to the presence of only hydroxyl (OH) and carboxyl (COOH) groups at the ends of the polyester molecules, while in nylon (for example) there is a relatively high frequency of amide (CONH) groups along the macromolecular chain. Therefore, this invention is primarily directed to polyester materials, and most particularly to adhesive-activated (AA) polyester fibers in cords, woven, knitted and non-woven fabrics used to reinforce conveyor belts, tires and hose.

5

10

15

20

25

30

Many adhesives and bonding systems ("dips") have been used for fabrics made from synthetic linear polyester yarns. Common systems like glycidyl ethers, phenolic condensates and blocked (or free) polyisocyanates are cost-ineffective and additionally suffer from various other disadvantages like precipitation and instability in baths in which fabrics are dipped. Usually, the fiber producers pre-treat the yarn with finish chemicals (e.g. silanes). Therefore, the resulting adhesive activated (AA) yarns provide an enhanced adhesion with a final adhesion system. This final adhesion system is most often based on RFL (Resorcinol-Formaldehyde-Latex). The adhesion surface on the cord is applied by its dipping in dispersions of RFL. Adhesion between cord and rubber is then achieved during curing with rubber.

Two examples of attempts to improve the adhesion of polyethylene terephthalate filaments to rubber are set forth in United States Patent 3,297,467 and 3,383,242. In these patents, polyethylene terephthalate filaments are treated with a spin finish which is an aqueous dispersion containing a polyglycidic ether of an acyclic hydrocarbon substituted by at least three hydroxyl groups or a diglycidic ether of an aliphatic diol, respectively, in combination with an amine curing agent and a lubricating agent. After heat treatment in order to bind the ether and amine components, the filaments or cord made therefrom can then be treated with an adhesive such as a RFL latex.

United States Patent 3,297,468 describes a similar finish except that the polyglycidic ether is of a cyclic hydrocarbon substituted with at least two hydroxyl groups.

Another example of an epoxide finish additive which may be employed to promote adhesion between a tire cord and an RFL adhesive is disclosed in United States Patent 3,803,035. The finish comprises a lubricating oil, an

antistatic agent, an emulsifier and a polyepoxide. Suitable antistatic agents include quaternary ammonium and pyridinium cationic agents.

United States Patent 3,911,422 and 3,968,304 are directed to a method of bonding polyester tire cords to rubber by use of a two-step process. In the first step, a dip is employed which comprises a low molecular weight polyallyl-glycidyl ether in an aqueous media. In the second step, a dip is employed comprised of an alkaline aqueous dispersion of a rubbery vinyl pyridine copolymer and a resinous composition reactive if exposed to heat.

5

15

Also see United States Patent 4,348,517 wherein the same epoxy ether silane is combined with the triglycidyl ether of a glycerol and a defined diglycidyl ether and is used as a fiber finish for polyester yarn.

United States Patent 3,793,425 also describes a process for improving the adhesion of polyester material to rubber. In the process, undrawn polyester yarn is coated with a composition containing an epoxy resin which is preferably buffered with an alkaline agent, such as sodium carbonate, lithium carbonate, potassium carbonate or ammonium hydroxide. The use of epoxy resins with alkaline catalysts to improve the adhesion of polyester to rubber is further disclosed in United States Patent 3,423,230 and United States Patent 3,464,878.

A process for treating chemically stabilized polyester material to improve the 20 adhesion of the polyester to rubber is also described in United States Patent 4,751,143. As noted therein, the aging period for chemically stabilized, adhesive activated polyester material can be reduced by contacting the material before it is substantially drawn or stretched with a composition containing a defined epoxide compound catalyzed with ions of at least one 25 of potassium, cesium, or rubidium at a pH of between about 7.5 to about 13.0. The application of finishes to the polymer surface generally produces a temporary surface condition such as lubrication or electrostatic charge dissipation which may be removed when the surface is subsequently exposed to multiple processing steps. Additionally, polyester surface 30 modifications of the prior art employing epoxies to improve the adhesion of polyester to rubber for example, have resulted in the use of a high level of chemical pick-up. Other approaches employed in art to adjust the characteristics or properties of organic polymer surfaces include electrolytic and plasma treatments. However, these processes are costly and have 35

limited processing rates. The application of a strong acid or base has not been particularly effective in modifying surfaces and can penetrate beyond the surface, particularly in fiber structures, to cause strength loss. Polyisocyanates have been employed to enhance adhesion in the manufacture of polyester yarns (see United States Patent 3,549,740). These materials have been applied at relatively high concentration levels (greater than 0.5 wt.-%) and so generate obnoxious vapors, produce deposits on process rolls and bond filaments to filaments in the yarn bundle. Similar processing problems are encountered in the application of known polyester adhesives such as those based upon resorcinol-formaldehyde resins described in United States Patent 3,660,202 and United States Patent 3,318,750.

5

. 15

20

25

United States Patent 4,078,115 discloses an adhesive system for bonding polyester filaments to rubber in which a first coating is employed comprised of the reaction product of a polyepoxide and a quaternized copolymer of 4-vinylpyridine and an aminimide. A second coating of an RFL adhesive is also employed.

Canadian Pat. No. 652,487 discloses a two coat adhesive system. One coat is a composition comprising triallyl cyanurate, the other a composition comprising vinyl pyridine copolymer RFL. The triallyl cyanurate is polymerized prior to bonding to the cord.

United States Patent 3,318,750 also discloses a two coat system. One coat is an aqueous solution of the reaction product of an aldehyde and a composition derived from the reaction of an unsaturated aliphatic ester of cyanuric acid and resorcinol, the other being a RFL dispersion. Optionally the second component can be just the rubbery copolymer latex. The total solid coating is 2% to 7%. This coating is cured, and the cord embedded in rubber and vulcanized.

United States Patent 3,419,463 and United States Patent 3,419,464 also use a reaction product of resorcinol, triallylcyanurate and formaldehyde ("N-3") as part of their adhesive system.

The application of RFL requires considerable expenditure and costs. The Cords are for example treated at high temperatures to cure the adhesive coating which leads to the consumption of a lot of energy, furthermore an

additional process step for the production of tires is needed. In addition the high temperature treating is used to control the balance of the physical properties, such as strength, modulus and shrinkage, of the treated cord.

In order to improve the adhesion further adhesion promoters are added to the rubber in addition to the RFL.

It is known from the prior art that by using a suitable adhesion promoter in sufficient amounts in the rubber formulation adhesion of cords to the rubber can be achieved without applying RFL (direct cord/rubber adhesion). A major disadvantage of this method is the large amount of adhesion promoter needed to achieve the desired effect. As a consequence, the rubber properties are determined to a large extend by the properties of the used adhesion promoter. The large amounts of adhesion-promoters to be used constitute a significant expense factor.

Objects and Summary of the Invention

5

- It is therefore a primary object of the present invention to provide an easily applicable and less material consuming method to achieve direct coating to a textile reinforcing fiber during the yarn processing steps. This method should render conventional dipping process as a separate manufacturing step unnecessary.
- A second object of the present invention is the provision of a coating composition which, if applied to the reinforcing material, leads coating (topcoat) providing for an increased adhesion of the coated textile reinforcing material to the rubber compared to the non-coated textile reinforcing material, for instance a yarn.
- A third object of the present invention is the provision of a textile reinforcing material having increased adhesion to rubber.
 - It is a fourth object of the present invention to provide a reinforced rubber article having improved dynamic fatigue properties.

The method according to the invention provides improved adhesion between a textile reinforcing material, e. g., the textile cord or a reinforcing member, and the rubber of a reinforced article, e. g., a tire, hose, V-belt or a conveyor belt.

Moreover, the method according to the invention leads to a reduction of production expenditure, since a pretreatment of reinforcing material such as a polyester yarn by dipping into adhesion promoters as a separate step during manufacturing, in addition to the elimination of the heat treatment step, is rendered redundant.

In a first embodiment the present invention relates to a method to achieve direct adhesion between a textile reinforcing material and an activated rubber comprising the steps of

5

10

- (A) applying an adhesion-imparting composition to the surface of the textile reinforcing material;
- (B) exposing the coated textile reinforcing material of step (A) to an elevated temperature;
- (C) embedding the coated textile reinforcing material of step (B) into an activated rubber; and
- (D) curing the reinforcing material containing rubber obtained from step (C) at a temperature and for a time sufficient to cure said rubber.

In a second embodiment the present invention relates to a coating composition comprising

- (i) a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and
- 25 (ii) a latex having a solids content from about 30 to about 50 wt.-%, preferably about 35 to about 45 wt.-%, most preferably about 41 wt.-%; wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

In a third embodiment the present invention relates to a textile reinforcing material obtainable by the method according to the present invention having improved adhesion to rubber. With regard of the present invention "improved adhesion" means that the force (determined according to ASTM 2229-99) which has to be used to pull out the embedded fibers of the

rubber is in the range of at least about 5 to about 10 N, preferably about 15 to about 35 N, most preferably about 20 to about 80 N.

In a fourth embodiment the present invention relates to a reinforced rubber article having improved dynamic fatigue properties. Latter means that the strength of the cords embedded measured after 10.6 million cycles (Disc fatigue test ASTM 6588) was not less than about 60 %, preferably not less than 70 %, most preferably not less than 95 %.

In contrast to the prior art, it has been surprisingly found, that improved adhesion between conventional adhesive activated polyester materials and conventional activated rubbers has been achieved without using conventional resorcinol formaldehyde resins and conventional processes such as dipping and heat treating.

Detailed Description of the Invention

5

10

30

According to the present invention the textile reinforcing material is preferably selected from organic polymeric materials such as polyesters, 15 polyamides, polycarbonates, polynitriles. The polyesters may be selected from any highly polymeric linear polyester obtained by heating one or more glycols of the series $HO(CH_2)_nOH$, wherein n is greater than 1, but does not exceed 10, with one or more dicarboxylic acid such as naphthalene 20 dicarboxylic acid, 4,4'-diphenyl dicarboxylic acid or preferably terephthalic acid, or an ester forming derivative thereof. Examples of ester forming derivatives of dicarboxylic acids are their aliphatic (including cyclo-aliphatic) and aryl esters and half-esters, its acid halides and their ammonium and salts. Examples of glycols are ethylene, trimethylene, tetramethylene, hexamethylene and decamethylene glycols. 25

Additionally, the polyester may be reacted or blended with compatible compounds or polymers which do not substantially adversely affect the characteristics of the polyester. For example, compounds yielding non-ester linkages can be added into the reaction mixture for the polyester or pigments, fillers, anti-oxidants, etc. can be blended with the polyester. The preferred polymer for purposes of this invention will be composed of at least about 85 wt.-%, preferably about 95 wt-% polyethylene terephthalate (PET)

or polyethylene naphthalate (PEN) and will most preferably be substantially all polyethylene terephthalate or polyethylene naphthalate.

The material into which the polyester is formed can be any size and configuration amenable to processing which will undergo adhesive activation. The material can therefore be filaments, yarns, cords, fabrics, tapes or films. Preferably, the material is filaments or yarn that is melt spun and quenched, particularly those intended for adhesion to rubber as in the production of tires. Illustrative of such polyester material is multifilament polyethylene terephthalate yarn, which is highly crystalline and highly orientated.

5

10

15

20

25

30

The preparation of such high crystalline and highly orientated yarn is, for example, set forth in United States Patent 4,414,169, the disclosure of which is fully incorporated herein by reference. An alternate process for preparing multifilament polyethylene terephthalate yarn is set forth in United States Patent 4,195,052, the disclosure of which is fully incorporated herein by reference.

The polyester material used in the present invention may or may not be chemically stabilized. Under typical preparation conditions, a polyester, such as polyethylene terephthalate, has a level of carboxyl end groups ranging from about 30 to about 40 microequivalents per gram. To obtain chemical stabilization of the polyester, a compound such as ethylene carbonate, phenyl glycidyl ether, or preferably ethylene oxide, is incorporated into the polyester material. For example, ethylene oxide can be added to a polyester melt which is maintained at a pressure of from about 3,548 kPa to about 35,480 kPa in accordance with the disclosures of United States Patents 4,016,142 and 4,442,058, the disclosure of each of which is fully incorporated herein by reference.

Although the invention is described in terms of the adhesive activating of polyester material, it will be appreciated that other polymers which may be activated by the present activator systems may likewise be treated. Such polymers include polyamides, especially aromatic polyamides (e.g., Kevlar), nylon, polycarbonate, rayon and other textile reinforcing fibers.

The term "filament" or "fiber", as used herein, refers to the components which make up a yarn.

The term "yarn", as used herein, is a generic term for a continuous strand of fibers, or filaments.

The term "cord" as used herein refers to a plurality of polyester filaments or yarns twisted together to form a single string or reinforcement element. In one illustrated embodiment, the cord comprises 2 to 3 yarns, has a linear density of dtex about 2200 to about 8800, a twist multiplier of about 2.0 to 7.5 (turns per meter/ $\sqrt{\text{dtex}}$).

The cord of the invention is preferably made of polyester such as polyethylene terephthalate (PET) or polyethylene naphthalate (PEN).

The polyester yarns applied in the present invention are preferably adhesive activated yarns having high-modulus-low-shrink (HMLS) properties. Such yarn having a high modulus, preferably less than about 5% elongation at a load of about 40 cN/tex. They are manufactured by high speed spinning followed by applying a finish comprising epoxy-compounds as described in GB-A-1012935, European published patent application 0420333 and United States Patent 3,775,150 or halohydroxy compounds as described in United States Patent 5,328,765, the disclosure of each of which is fully incorporated herein by reference. Afterwards the yarn is drawn and heat-treated.

20 (A) Application of the Topcoat

5

The textile reinforcing material is coated on its surface by contacting the material after it has been drawn and/or heat set with a coating composition comprising

- (i) a resin obtainable by the reaction of triallyl cyanurate and resorcinol at temperatures from about 180 to about 280°C, preferably about 200 to about 260°C, most preferably about 220 to about 240°C then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia;
 - (ii) a latex;

wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

The coating composition can be an aqueous, a non-aqueous or an emulsion composition which comprises at least one polymerizable component. The reinforcing material is surface-treated/coated with said coating composition thus forming a top-coat which, after the removal/evaporation of the solvents leaves behind a coating on the surface of the reinforcing material which gives raise to an improved adhesion to rubbers, in particular activated rubbers.

5

10

Suitable resin components (i) are well known in the art under the designation "N-3", e.g. from United States Patent 3,318,750 and 3,419,464 and Canadian patent application 652,487, the disclosure of each of which is fully incorporated herein by reference.

The latex component (ii) of this invention should not be considered as being limited to any specific type of synthetic rubber latex, but rather to include all of those comparable diene polymer latex compositions commonly employed in the rubber fabricating industry. It is preferred however, that the latex contains at least some vinyl pyridine latex. This well-known type of latex is formed from butadiene, styrene, and vinyl pyridine monomers, in a ratio of about 50 to about 80 wt.-% of butadiene, about and about 10 to about 25 wt.-% of vinyl pyridine monomers, usually in a ratio of about 70/15/15 wt.-%.

The coating composition may further comprise a lubricant, such as butyl stearate, ethoxylated long chain alcohols, ethoxylated polysiloxanes and mixtures thereof, in amounts ranging from about 0 to about 1% by dry weight.

- The coating composition may also comprise a solvent, such as water, acetone, butyl carbitol, isopropanol, ethanol and mixtures thereof. The preferred solvent is water in an amount ranging from about 1 to about 99 %, preferably about 50 to about 95 % by weight. Water is advantageously employed as the solvent for a composition used as a coating on drawn yarn.
- Other components which may be present in the coating composition include tints, fluorescent brighteners, emulsifiers, antifoaming agents, antimicrobial compounds, co-catalysts, flexibilizers such as methacrylates and mixtures thereof. The total amount of solids (i.e., all constituents except solvent) in

the topcoat composition typically ranges from about 1 to about 90% by weight, preferably from about 1 to about 50% by weight.

The coating composition can be applied to the polymeric material using any suitable means which is selected primarily based on the form of the material. Exemplary means include a metered applicator, a kiss roll, spray or foam and results in a coating level with increasing preference in the order given of at least about 0.01, 0.05, 0.1 % by weight. The coating level can be – with increasing preference in the order given – up to about 3 %, 2 %, 1.5 % and 1% by weight, based on the weight of the dry coated textile reinforcing material.

Polymerizing Step (B).

5

10

15

20

25

30

After applying the coating composition to the drawn yarn or cord it is at least partially polymerized by exposing it to an elevated temperature sufficiently high to polymerize polymerizable constituents contained in the coating composition. It is preferred to expose the coated textile reinforcing material to a temperature of from about 110 to 235° C. The exposure time at lower temperatures is several minutes, at higher temperatures it is about 60 seconds or less. At least partially polymerizing means in accordance with the present Invention that at least about 5 to about 50 mol-%, preferably about 10 to about 30 mol-%, most preferably about 15 to about 25 mol-% of the monomers are linked with each other. Optionally this polymerization step can be conducted in the normal treating process.

Curing Step (C)

After at least partially polymerizing the coating composition the coated textile reinforcing material embedded into the rubber matrix resulting in an adhesion of the rubber to the reinforcing material. Therefore, the coated polymeric reinforcing material, for instance, a polyester cord/yarn is embedded in a curable rubber and the rubber is cured for about 6 to 120 min, preferably for about 6 to about 15 min., most preferred for about 6 to about 10 min. at temperatures of about 160 to about 200°C, preferably of about 160 to about 190°C, most preferred of about 170 to about 180°C.

In a preferred embodiment of the present invention the rubber employed is an activated rubber, i.e., a rubber formulation which comprises agents

known from the prior art for improving the adhesion to RFL treated cord. Specific examples for said rubber adhesion promoters are resorcinol, hexamethoxymethyl melamine (HMMA), sulfur, sulfenamides, zinc oxide, stearic acid and carbon black.

The term "rubber" as used herein refers to carbon black and/or silica filled 5 natural and synthetic rubber systems, which can be cured so as to exhibit elastomeric properties. For the purpose of this invention the term "elastomer" is used interchangeably with the term "rubber". Representative synthetic rubbery polymers include the diene polymers. Diene polymers comprise those polymers having rubber-like properties which are prepared 10 by polymerizing a conjugated C_4 to C_6 diolefin such as butadiene, isoprene chloroprene copolymerized with styrene, methyl styrene and acrylonitrile, the conjugated diolefin usually being present in the mixture to the extent of at least about 40 wt.-% - based on the total of polymerizable material - and preferably in major portion. The butadiene-styrene copolymers are 15 manufactured commercially under such names as SBR 1000, SBR 1006, SBR 1500 and 1502.

Other synthetic rubbers include the "neoprene" rubbers. "Neoprene" is a generic name which is applied to polymers of chloroprene, and copolymers of chloroprene with dienes or vinyl compounds, in which the chloroprene comprises the predominant monomer. An isobutylene-isoprene copolymer "Butyl" rubber, as well as the elastomeric ethylene-propylene copolymers and terpolymers may also be used.

20

The term "cured" is used interchangeably with the term "vulcanized" in conjunction with the cured rubber component of this invention denotes that the rubber component to be vulcanized has been cured to a state in which the physical properties of the rubber are developed to impart elastomeric properties to the rubber generally associated with the rubber in its conventional vulcanized state.

The rubber employed may contain customary amounts of various conventional additives such as those needed to effect or accelerate vulcanization. Examples of such materials include sulfur, sulfur chloride, sulfur thiocyanate, thiuram polysulfides and other organic or inorganic polysulfides. These components are preferably employed in amounts

varying from about 0.1 to about 10 wt.-% and preferably from about 0.3 to about 3 wt.-% of rubber.

Many other materials may also be included in the rubber composition such as pigments, antioxidants and the like, all in accordance with practices well known in the art.

The following Examples are given as illustrations of the invention. It should be understood, however, that the invention is not limited to the specific details set forth in the Examples.

The following examples are presented to illustrate the invention which is not intended to be considered as being limited thereto. In the examples and throughout percentages are by weight unless otherwise indicated.

While in accordance with the patent statutes, the best mode and preferred embodiment have been set forth, the scope of the invention is not limited thereto, but rather by the scope of the attached claims.

15 Examples

5

Commercial HMLS tire yarns from KoSa were used for the Examples. Type 792 is a non-adhesive activated yarn, Type 793 is an adhesive activated (AA) (halohydroxy based) yarn and Type 748 is another adhesive activated yarn (epoxy based).

20 The topcoat composition (N3-L) used in the examples was

35.7 wt.-% butadiene/styrene/vinylpyridine terpolymer (Gentac 118® from Omnova Solutions Inc., Mogadore Ohio, USA);

35.7 wt.-% N-3® from FCI Technology Inc. Bessemer City, North Carolina, USA.

25 28.6 wt.-% Water

The yarns or cords were coated to a total level of finish on yarn, unless otherwise stated, of 1.0 wt.-% on a dry weight basis.

The coated/treated yarns or cords were heated at 229° for 60 seconds, unless otherwise stated. The rubbers used in the examples were Rubber A a non-activated rubber (without resorcinol and formaldehyde and Rubber B an activated rubber (containing resorcinol and formaldehyde).

Example 1

1440 dtex Type 792 and 793 yarns were twisted into a 2 ply cord with a twist multiplier of 6. These cords were coated and partially polymerized for 55 seconds at 235° C and then embedded in both activated and non-activated rubbers and cured at 150° C for 30 minutes. The force to pull out the cords was measured according to ASTM 2229-99, and the results set forth in Table 1.

Table 1

10

15

20

5

Yarn (PET)	Rubber	Pull-out Adhesion (N)
792 (non-AA)	Α	15
792 (non-AA)	В	25
793 (AA)	Α	20
793 (AA)	В	65-85

The results in table 1 demonstrate that the combination of AA-Yarn and activated Rubber B lead to a significant increase of adhesion level. The results of 792 yarn in Rubber A represent the prior art of United States Patent 3,318,750.

Only if the rubber contains an adhesion promoter and the cord contains an active finish, significant levels of adhesion could be observed in the pull-out test.

In accordance to the present invention it has been observed, that it was sufficient to use a standard topcoat (on the yarn) and small amounts of a standard adhesion system in the rubber to achieve good adhesion. The topcoat is interacting directly with the rubber and not via the RFL.

Example 2

The adhesion of the inventive system was compared to conventional RFL dipping. Fabrics (121 epdm) were prepared from Type 793 and Type 748

cords. Both the 793 and 748 fabrics were coated with the N3-L topcoat and partially polymerized prior to the fabric being embedded in activated rubber B. One length of 793 fabric was not coated, and another dipped in a standard RFL composition with a 5% dip pick-up and cured. The rubber composite was cured for 10 min. at 177°C. The peel adhesion (ASTM 4393) of these composites is set forth in Table 2.

This example shows that the cord material obtained from coated yarns has equivalent adhesion forces compared to standard RFL dipped cords. In addition, the coated samples show a significant adhesion improvement compared to the non-coated sample.

Table 2

Yarn in Fabric	Peel Adhesion Force (N)
793 (non-coated)	65-98
793 (coated)	135-152
793 (dipped)	132-178
748 (coated)	145-159

Example 3

10

15 The fabrics for Example 2 were used to build 205/60 R15 tires. The peel adhesion of sections cut from the sidewalls was measured and the results set forth in Table 3.

Table 3

Yarn in Fabric	%Rubber Coverage	Adhesion (N)
793 (non-coated)	0	38-46
793 (coated)	10	42-54
793 (dipped)	70	53-60
748 (coated)	80	72-81

Table 3 shows the in-tire adhesion performance of calendered carcass fabrics. With all activated Rubber B skim compound the cured tire shows, under equivalent curing conditions, that coated and dipped carcass sections show equivalent adhesion performance, and low adhesion values in the case of tires built with non-coated 793. Best results for rubber coverage shows in tire cord fabric manufactured with coated 748 (AA) yarn.

Testing of these tires, high speed, endurance and durability in the flexing zone showed no difference between the fabrics.

Example.4

The effect of the curing conditions on the final adhesion (pull-out force) between rubber and cord was measured using cords from Example 1, and the results set forth in Table 4. As is evident from the results, longer curing-times and higher temperatures are beneficial to achieve higher adhesion. Preferably, curing temperatures of 160-200°C are applied, the cure time may be varied between 6-120 min.

Table 4
Pull-out Adhesion (N)

Yarn	Curing Conditions (in Rubber B)						
	30 min @150°C	i .	12 min	15 min	8 min	12 min	15 min @180°C
793	34	33	53	65	44	54	55
748	45	43	73	78	70	92	86

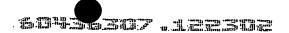
5 Example 5

The topcoat was applied at various stages of the process:

- A) Yarn coated and then twisted into 2-ply cord
- B) Yarn twisted into a single ply, coated and twisted into a 2-ply cord
- C) Cord coated
- 10 The cords were partially polymerized, embedded in rubber B and cured. The peel force of the cured rubber was measured and the results set forth in table 5.

Table 5

Application process	Yarn Type	Pull-out Adhesion (N)
Α	793	30
В	793	40
c	793	62
Α	748	72
В	748	30
C ·	748	93



The preferred method for applying the topcoat is either at the yarn or cord stage.

Example 6

5 1440 dtex Type 748 yarns were coated with 0.6wt.% of N3-L, and partially polymerized for 11 seconds at 220° C. The yarns were twisted into 2-ply cords at a low twist level of 250. Control cords from the same yarn were prepared at different twist levels and dipped in a standard RFL dip composition with a 5% dip pick-up and cured in a treating oven. These cord were embedded in the activated Rubber B and cured at 150° C for 30 minutes.

Visual inspection of the cords after a peel adhesion test showed excellent adhesion of the cords (visual ratings of 4.5 to 5).

The embedded cords were subjected to a dynamic fatigue test (Disc fatigue test ASTM 6588), and the strength of the cords measured after 3.6 and 10.6 million cycles. The results are set forth in Table 6 below.

Table 6

Adhesion System	Twist level (Turns/meter)	Retained strength, % (Number of cycles)	
-		3.6 million	10.6 million
RFL	370	100	94
RFL	310	92	82
RFL	250	75	47
N3-L	250	95	70

20

This demonstrates the superior dynamic fatigue of the inventive system, and will allow lower twist levels to be used in rubber composites.

What is claimed is:

5

- A method to achieve direct adhesion between a textile reinforcing material and an activated rubber comprising the steps of
 - (A) applying an adhesion-imparting composition to the surface of the textile reinforcing material;
 - (B) exposing the coated textile reinforcing material of step (A) to an elevated temperature;
 - (C) embedding the coated textile reinforcing material of step (B) into an activated rubber; and
- (D) curing the reinforcing material containing rubber obtained from step (C) at a temperature and for a time sufficient to cure said rubber.
- The method of claim 1 wherein the adhesion-imparting composition is
 an aqueous composition.
 - 3. The method of claim 1 wherein the adhesion-imparting composition comprises at least one polymerizable component.
- 20 4. The method of claim 1 wherein the textile reinforcing material is an organic polymeric material.
- The method of claim 4 wherein the textile reinforcing material is selected from the group of aliphatic and aromatic polyesters, polyamides, polycarbonates and rayon.
 - 6. The method of claim 1 wherein the coated textile reinforcing material is exposed to a temperature in the range of from about 110°C to about 250°C;

- 7. The method of claim 1 wherein the rubber is selected from the group consisting of diene rubbers, diene/alpha-olefin rubbers, ethylene/propylene rubbers and ethylene/alpha-olefin/diene rubbers.
- The method of claim 1 wherein the rubber is cured at a temperature of from about 140°C to 220°C, preferably from about 160°C to 200°C, most preferably from about 170°C to 180°C.
- 9. The method according to claim 1, wherein the adhesion-imparting composition comprises

į

15

- i. a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and
- ii. a latex having a solids content from about 30 to about 50 wt.-%, preferably about 35 to 45 wt.-%, most preferably about 41 wt.-%

wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

- 10. A treating composition for imparting adhesion to reinforcing materials said composition comprising
- i. a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and
- ii. a latex having a solids content of from about 30 to about 50 wt.-%, preferably about 35 to 45 wt.-%, most preferably about 41 wt.-%

wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

- 5 11. A textile reinforcing material obtainable by a method comprising the steps of
 - (A) applying an adhesion-imparting composition to the surface of the textile reinforcing material; and
- (B) exposing the coated textile reinforcing material of step (A) to an elevated temperature.
 - 12. The material of claim 11 wherein the adhesion-imparting composition is an aqueous composition.
- 15 13. The material of claim 11 wherein the adhesion-imparting composition comprises at least one polymerizable component.

20

- 14. The material of claim 11 wherein the textile reinforcing material is an organic polymeric material.
- 15. The material of claim 14 wherein the textile reinforcing material is selected from the group of aliphatic and aromatic polyesters, polyamide, polycarbonate and rayon.
- 25 16. The material of claim 11 wherein the coated textile reinforcing material is exposed to a temperature in the range of from about 110°C to about 250°C;
- 17. The material of claim 11 wherein the adhesion-imparting composition30 comprises

- i. a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and
- ii. a latex having a solids content from about 30 to about 50 wt.-%, preferably about 35 to 45 wt.-%, most preferably about 41 wt.-%
- wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

5

30

- 18. The material of claim 11 wherein the adhesive coating is present in an amount of from about 0.01 to about 3 % by weight, preferably from about 0.05 to about 2 % by weight, and most preferably from about 0.1 to about 1.5 % by weight, based on the weight of the dry coated textile reinforcing material.
- 19. A reinforced rubber article having improved dynamic fatigue
 20 properties obtainable by a method comprising the steps of
 - (A) applying an adhesion-imparting composition to the surface of the textile reinforcing material;
 - (B) exposing the coated textile reinforcing material of step (A) to an elevated temperature;
- (C) embedding the coated textile reinforcing material of step (B) into an activated rubber; and
 - (D) curing the reinforcing material containing rubber obtained from step (C) at a temperature and for a time sufficient to cure said rubber.

20. The article of claim 19 wherein the adhesion-imparting composition is an aqueous composition.

- 21. The article of claim 19 wherein the adhesion-imparting composition comprises at least one polymerizable component.
- 5 22. The article of claim 19 wherein the textile reinforcing material is an organic polymeric material.
- 23. The article of claim 19 wherein the textile reinforcing material is selected from the group of aliphatic and aromatic polyesters,
 polyamides, polycarbonates and rayon.
 - 24. The article of claim 19 wherein the coated textile reinforcing material is exposed to a temperature in the range of from about 110°C to about 250°C;

25. The article of claim 19 wherein the rubber is selected from the group consisting of diene rubbers, diene/alpha-olefin rubbers, ethylene/propylene rubbers and ethylene/alpha-olefin/diene rubbers.

15

30

- 20 26. The article of claim 19 wherein the rubber is cured at a temperature of from about 140°C to 220°C, preferably from about 160°C to 200°C, most preferably from about 170 °C to 180°C.
- 27. The article according to claim 19, wherein the adhesion-impartingcomposition applied comprises
 - i. a resin having a solids content from about 10 to about 50 wt.-%, preferably from about 15 to about 30 wt.-%, most preferably from about 20 wt.-% obtainable by the reaction of triallyl cyanurates and resorcinol at high temperatures, then reacting the resulting product with formaldehyde and solubilizing it in aqueous ammonia; and

ii. a latex having a solids content from about 30 to about 50 wt.-%, preferably about 35 to 45 wt.-%, most preferably about 41 wt.-% wherein the weight-ratio of resin (i) to latex (ii) is from about 50/50 to about 80/20, based on the total weight of (i) and (ii).

5 -

10

28. The article of claim 19 wherein the adhesive coating is present in an amount of from about 0.01 to about 3 % by weight, preferably from about 0.05 to about 2 % by weight, and most preferably from about 0.1 to about 1.5 % by weight, based on the weight of the dry coated textile reinforcing material.

Abstract

Improving Adhesion between Textile Reinforcing Materials and Rubber

The present invention relates to a method for improving direct adhesion between a textile reinforcing material and an activated rubber. Moreover, the invention relates to a coating composition, a yarn, cord or fabric manufacturing process which is used for the method according to the invention, a textile reinforcing material obtainable by said method having increased adhesion to rubber and a reinforced rubber article having improved dynamic fatigue properties.

This Page is Inserted by IFW Indexing and Scanning Operations and is not part of the Official Record

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

□ BLACK BORDERS
□ IMAGE CUT OFF AT TOP, BOTTOM OR SIDES
□ FADED TEXT OR DRAWING
□ BLURRED OR ILLEGIBLE TEXT OR DRAWING
□ SKEWED/SLANTED IMAGES
□ COLOR OR BLACK AND WHITE PHOTOGRAPHS
□ GRAY SCALE DOCUMENTS
□ LINES OR MARKS ON ORIGINAL DOCUMENT
□ REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY

IMAGES ARE BEST AVAILABLE COPY.

☐ OTHER:

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.